

SCREEN SUPPLY AND NEGATIVE BIAS FOR THE 4CX250B H.F. AMPLIFIER.

FOR MY SCREEN & GRID POWER SUPPLIES, I DECIDED TO ADOPT SOME OF GEORGE T. DAUGHTERS, K6GT IDEAS AND INCORPORATE ^{THEM} INTO MY OWN AMPLIFIER. HIS AMPLIFIER & SUPPLY, THE SUNNYVALE/SAINT PETERSBURG KW PLUS IS FEATURED IN CHAPTER 18 OF THE 2005 ARRL HANDBOOK, AND PROVIDES AN EXCELLENT SOURCE OF REFERENCE FOR GOOD, PRACTICAL POWER SUPPLY CIRCUITRY.

ALTHOUGH I CHOSE TO USE A PAIR OF 4CX250B'S INSTEAD OF A 4CX1600B, THE GRID BIAS ARRANGEMENT ^{STILL} REQUIRES NEGATIVE ^{CONTROL} GRID AND POSITIVE SCREEN GRID SUPPLIES. FINDING AN APPROPRIATE TRANSFORMER AT A REASONABLE PRICE WAS THE CHALLENGE AND CHEAP PLUS DEPENDABLE EQUALS GOOD.

A FIXED, REGULATED SCREEN SUPPLY OF +300 VOLTS AT ABOUT 20 mA AND AN ADJUSTABLE ^{CONTROL GRID VOLTAGE SUPPLY} (UP TO) -90 VOLTS AT ABOUT 5 mA WAS CHOSEN. WAS A DESIGN PARALLEL.

MY JUNK BOX REVEILED A NEW TRIAD N-470A ISOLATION XFMR WITH TWO - 220 VOLT PRIMARIES AND ONE - 115 VOLT SECONDARY RATED AT 150 VA. THIS TRANSFORMER COULD EASILY BE RECONFIGURED TO PROVIDE BOTH SCREEN & CONTROL GRID VOLTAGES BY USING ONLY ONE OF THE PRIMARY WINDINGS AT A REDUCED VOLTAGE (120 VOLTS INSTEAD OF 220 VOLTS) FOR THE INPUT. THE OTHER PRIMARY WOULD BE CONNECTED TO A VOLTAGE DOUBLER CIRCUIT FOR THE SCREEN SUPPLY. NO LOAD VOLTAGE ^{AT THE} BEFORE ^{FILTERS} REGULATION WAS MEASURED AT +330 VOLTS; RESISTOR R_x

IS CURRENT LIMITING FOR THE FILTER CAPACITORS.
THE 115VAC ^{WINDING} IS CONNECTED TO A HALF-WAVE RECTIFIER FOR THE NEGATIVE GRID SUPPLY:

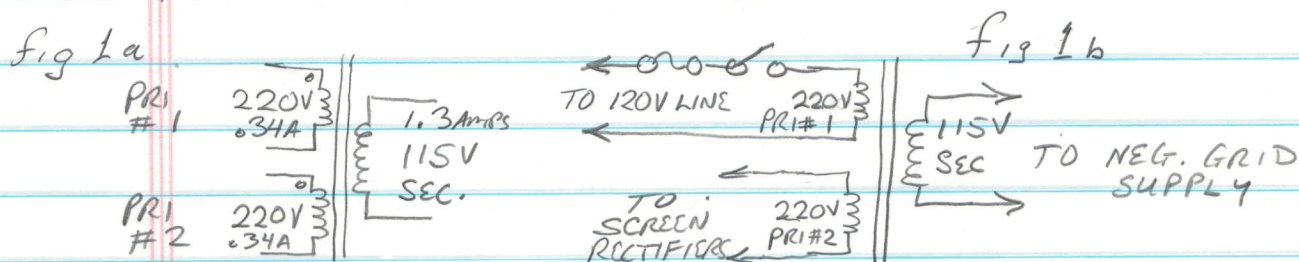


fig 1a SHOWS THE ISOLATION XFMR AND ITS WINDING.

PRIMARY # 1 CAN BE CONNECTED TO PRI # 2 WINDING IN EITHER PARALLEL CONFIGURATION FOR 220 VOLT INPUT OR SERIES CONNECTED FOR 440 VOLT INPUT. OUT PUT WOULD REMAIN 115VAC @ 150 VA.

IN KEEPING IN MIND THAT POWER XFMRs ARE RATED IN VA (VOLTS X AMPS), IF ONE WERE NOT TO EXCEED EITHER VOLTS OR AMPS, ONE COULD RE-CONFIGURE THE SAME TRANSFORMER AS IN fig 1b. NOTE THAT THERE ARE TWO PRIMARY WINDINGS RATED AT 220 VOLTS EACH. THE TRANSFORMER IS RATED FOR A TOTAL of 150 VA.

THEREFORE: PRI VOLTS X PRI AMPS = SEC VOLT X SEC AMPS OR

$$\text{EX: } 220 \text{ VOLTS} \times 0.68 \text{ AMPS} = 150 \text{ VA}$$

$$\text{FOR TWO PARALLEL WINDINGS: PRI VOLTS} \times \frac{\text{LINE AMPS}}{2} = \text{VA}$$

$$\text{EX: } 220 \text{ VOLTS} \times \frac{0.68}{2} = 150 \text{ VA}$$

EACH PRI. WINDING IS THEREFORE RATED FOR A MAXIMUM of 0.34 AMPS @ 220 VOLTS or 75 VA.

IF WE WERE TO REDUCE THE INPUT VOLTAGE FROM 220V TO 120 VOLTS; AND WERE TO USE ONLY ONE OF THE PRIMARY WINDINGS, THE TRANSFORMERS' MAXIMUM

VA RATING WOULD BE AS FOLLOWS:

$$\text{VOLTS INPUT (NOMINAL)} \times I_{\text{MAX}} = \text{NEW MAX VA RATING}$$

$$\text{EX: } 120\text{V} \times 0.34\text{AMPS} = 40.9\text{VA}$$

IF WE ARE CAREFUL NOT TO EXCEED THE ABOVE NEW VA RATING FOR THE TOTAL OF ALL WINDINGS, WE COULD USE THIS XFMR WITHOUT A PROBLEM.

AGAIN, HERE'S WHAT'S NEEDED:

$$+300\text{VDC AT } 2.0\text{mA} = V \times A = 300\text{V} \times 0.02\text{A} = 6\text{VA}$$

$$\text{AND } -90\text{VDC AT } 5\text{mA} = V \times A = 90\text{V} \times 0.005\text{A} = 0.45\text{VA}$$

THIS WOULD EQUATE TO A TOTAL OF LESS THAN 10VA.

PROVIDED WE DON'T EXCEED ANY SINGLE WINDINGS VA OR TOTAL RECONFIGURED PRIMARY VA, THIS XFMR WOULD FIT THE BILL WITH VA TO SPARE! BUT WE NEED TO DO THE MATH.

LET'S LOOK AT THE WINDINGS AGAIN:

$$\text{PRI \#1 RATED @ } 220\text{V} / 0.34\text{A} = 75\text{VA}$$

$$\text{WILL BE OPERATED AT } 120\text{V} / 0.34\text{A} = 40.9\text{VA (MAX)}$$

$$\text{PRI \#2 RATED @ } 220\text{V} / 0.34\text{A} = 75\text{VA}$$

$$\text{WILL PROVIDE THROUGH VOLTAGE DOUBLER: } 300\text{V} / 0.02\text{A} = 6\text{VA}$$

$$\text{EX } \frac{V_{\text{DC}}}{V_{\text{AC}}} = \frac{I_{\text{AC}}}{I_{\text{DC}}} \quad \text{OR} \quad \frac{300\text{V} \times 0.02\text{A}}{120\text{V}} = \frac{I_{\text{AC}}}{?}$$

$$\text{DIVIDE EACH SIDE BY } 120\text{V} \rightarrow \frac{300\text{V} \times 0.02\text{A}}{120\text{V}} = ? = 0.050\text{A}$$

NOTE THAT THE PRI #2 ^{WINDING} ~~THIS~~ CURRENT EXCEEDS IT'S RATING BY

ABOUT 16mA. ^{REMEMBER ALLOWABLE} MAX SCREEN DISIPATION FOR TUBE = 12W @ 400VDC

$$P = E \times I = 12\text{W} = 400 \times I \quad \frac{12}{400} = I = 30\text{mA MAX}$$

I EXPECT THE AVG SCREEN GRID CURRENT TO BE 1

$$\frac{I_{\text{MAX}}}{1.4} = \frac{0.03\text{A}}{1.4} = 21\text{mA} \times 300\text{VOLTS} \text{ OR } 6.3\text{WATTS} \times 2\text{TUBES} = 12.6\text{W}$$

THE AVERAGE SCREEN CURRENT AT FULL OUTPUT WOULD

BE:

- 1) $\frac{DC \text{ VOLTAGE} \times \text{CURRENT}}{AC \text{ WINDING VOLTS RMS}} = AC \text{ WINDING CURRENT PEAK}$
- 2) $\frac{AC \text{ WINDING CURRENT}}{1.4} = \text{AVG CURRENT}$

EX: 1) $\frac{300V \times 0.02A}{120V} = \frac{6}{120} = 0.05A \text{ PEAK}$

2) $\frac{0.05A}{1.4} = 36mA \text{ (SECONDARY WINDING CURRENT)}$

36mA WOULD BE THE AVG CURRENT DRAW AT FULL OUTPUT WITH 50mA PEAKS. THE TRANSFORMER WINDING IS RATED AT 34mA AND WOULD PROBABLY NOT HAVE ANY PROBLEM WITH THIS CIRCUIT CONFIGURATION

AN ALTERNATIVE WOULD BE TO USE A DUAL PRIMARY/
DUAL SECONDARY TRANSFORMER (THESE ARE ^{ACTUALLY} MORE COMMON)
CONNECT THE SECONDARIES IN SERIES
AND USE A FULL-WAVE BRIDGE INSTEAD OF A
VOLTAGE DOUBLER. THIS WOULD GIVE YOU TWICE THE
AVAILABLE POWER. AS ^{IN} THE FIRST EXAMPLE.

EX. 1) $\frac{300V \times 0.02A}{240V \text{ SEC}} = \frac{6VA}{240V} = 0.025A \text{ PK}$

2) $\frac{0.025A}{1.4} = 18mA \text{ (SECONDARY WINDING CURRENT)}$

WITH 16mA LEFT TO SPARE!

YOUR JUNK BOX COULD BE YOUR BEST FRIEND, DON'T BE AFRAID TO EXPERIMENT & DO THE MATH!

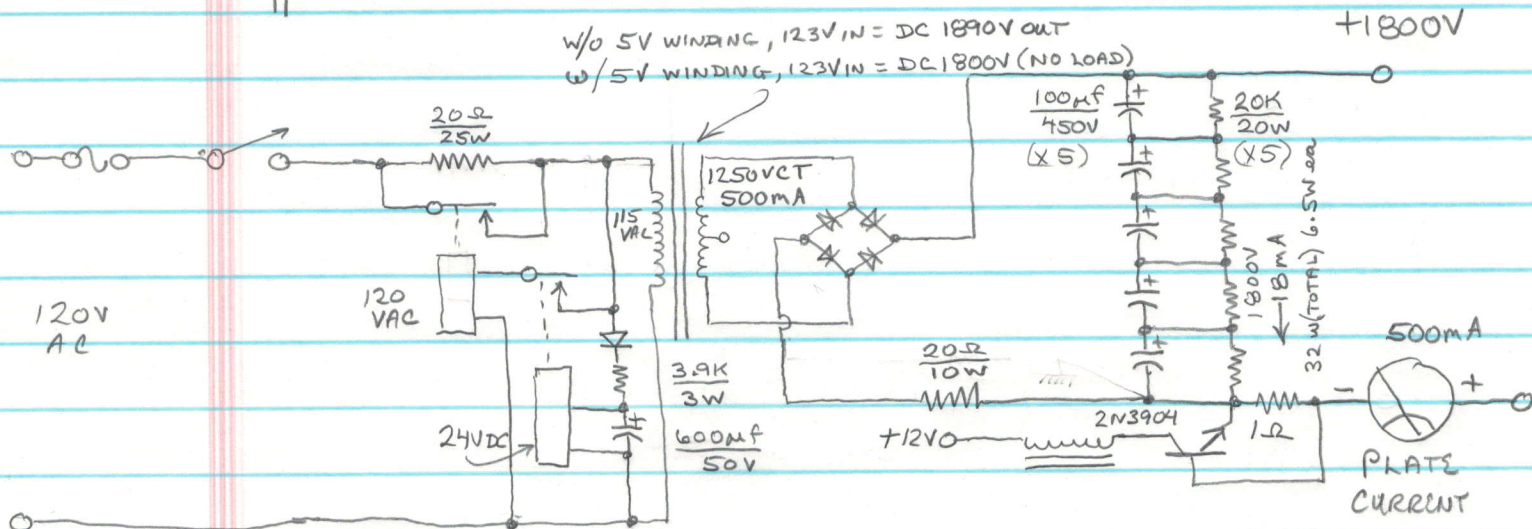
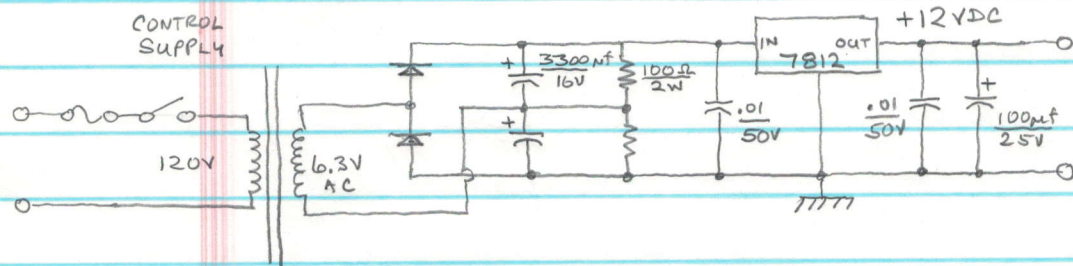
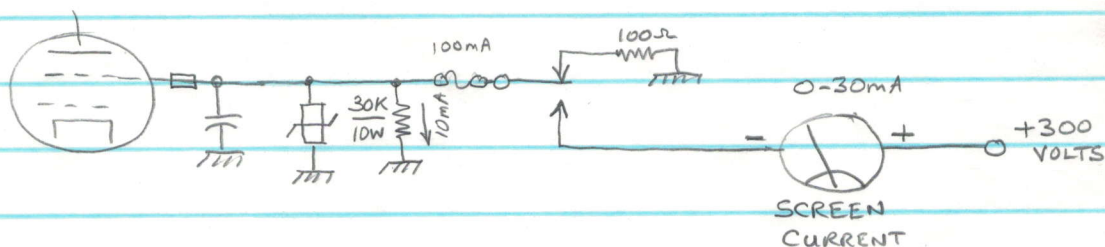
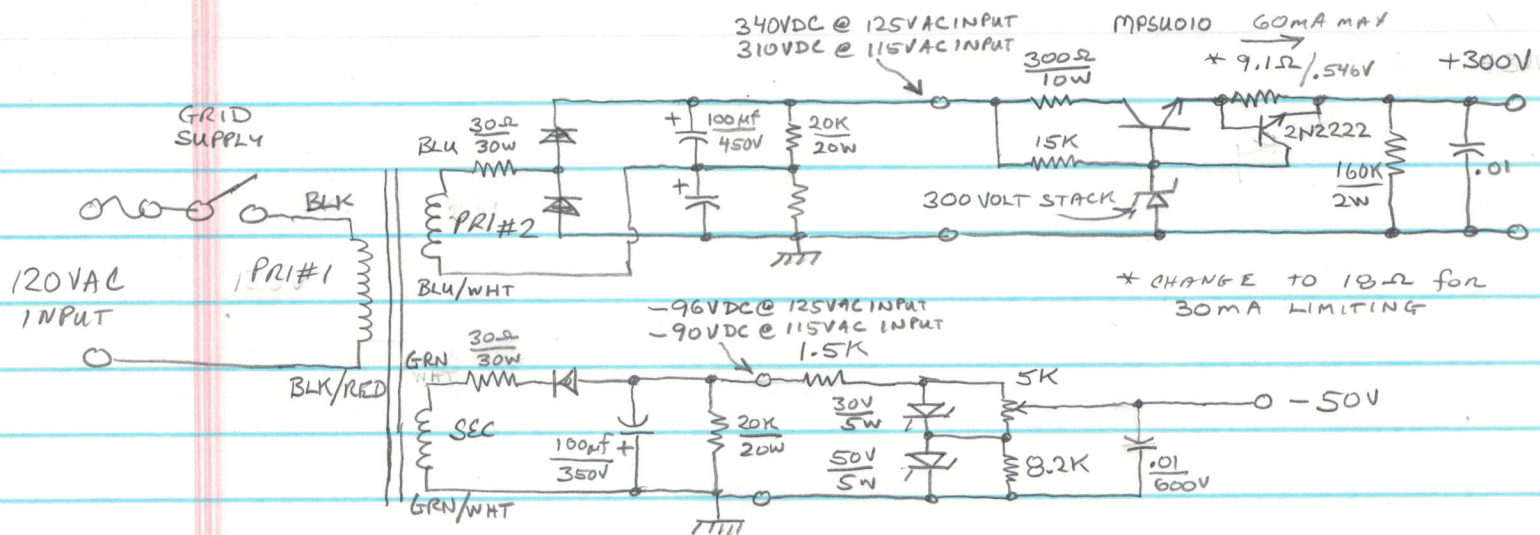
LET'S FINISH-UP WITH THE CONTROL GRID: (SECONDARY #1)

RATIO = $220V \times 0.68A = 115V \times 1.3A = EXI = EXI$

$120V \times 0.68 = ? \times 1.3A$

$\frac{81.6VA}{1.3A} = 62.8VAC \text{ RMS SEC WINDING VOLTAGE, } W/120V \text{ AC INPUT}$

$62.8 \times 1.6 (\text{RECTIFIER}) = \approx 100VDC$



WOO APPARATUS 4CX250A AMPLIFIER

PRELIMINARY EXPERIMENTS

