

ENGINEERING SKETCH PAD

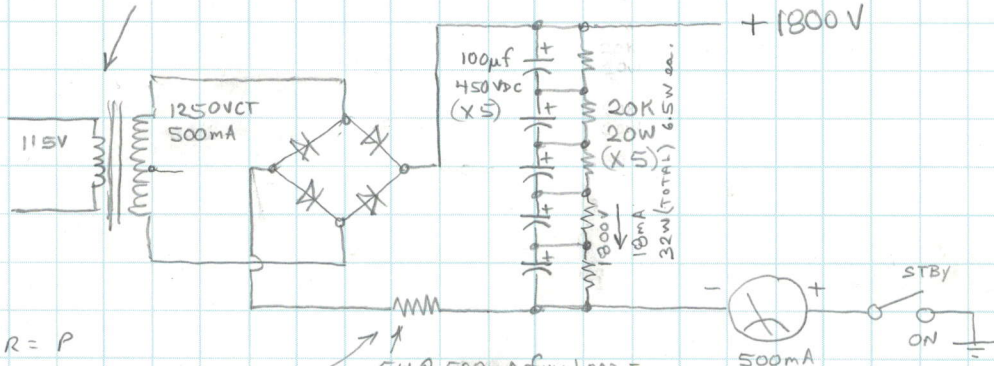
BY:	DATE:	SUBJECT:	SHEET NO.:
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			JOB NO.:

RCA XFMR (FILAMENT)

NO/5V WINDING, 123V IN = DC 1890V out

W/5V WINDING 123V IN = DC 1800V (NO LOAD)

PLATE SUPPLY

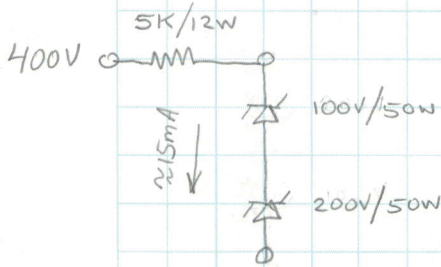


$$I^2 R = P$$

$$\frac{.5^2 R}{.5^2} = \frac{5}{.25} = 20\Omega, P = 5W < 10 \text{ VOLT DROP} >$$

$$\text{if } 50\Omega, P(W) @ 500mA = .5^2 \times 50 = 12.5W < 25 \text{ VOLT DROP} >$$

* TURN-ON CURRENT PULSE = 6mS @ 175 Volts ACROSS 50Ω = 3.5Amps

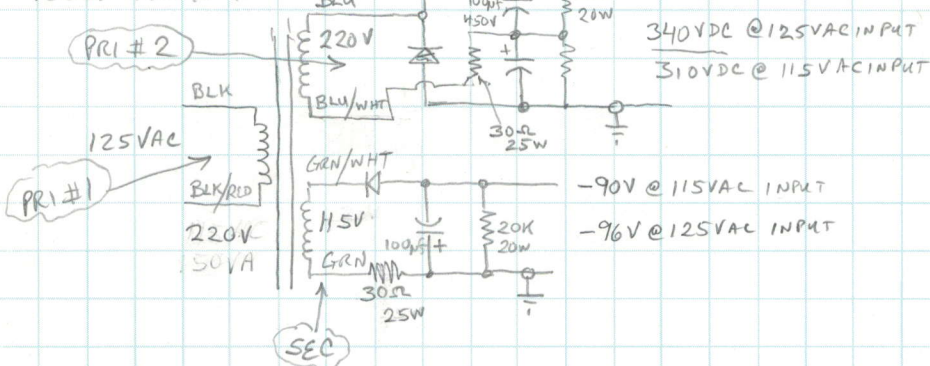


$$P = I^2 R = E \times I = \frac{E^2}{R} / 50W = \frac{100^2}{R} = \frac{100^2}{50} = 200\Omega / 10W = \frac{100^2}{10W} = R = 1000\Omega$$

$$50W = \frac{200^2}{R} = R = \frac{200^2}{50} = 800\Omega / 10W = \frac{200^2}{R}, R = \frac{200^2}{10} = 4K\Omega$$

$$50mA \text{ max} = 4K\Omega \times .05^2 = 10W$$

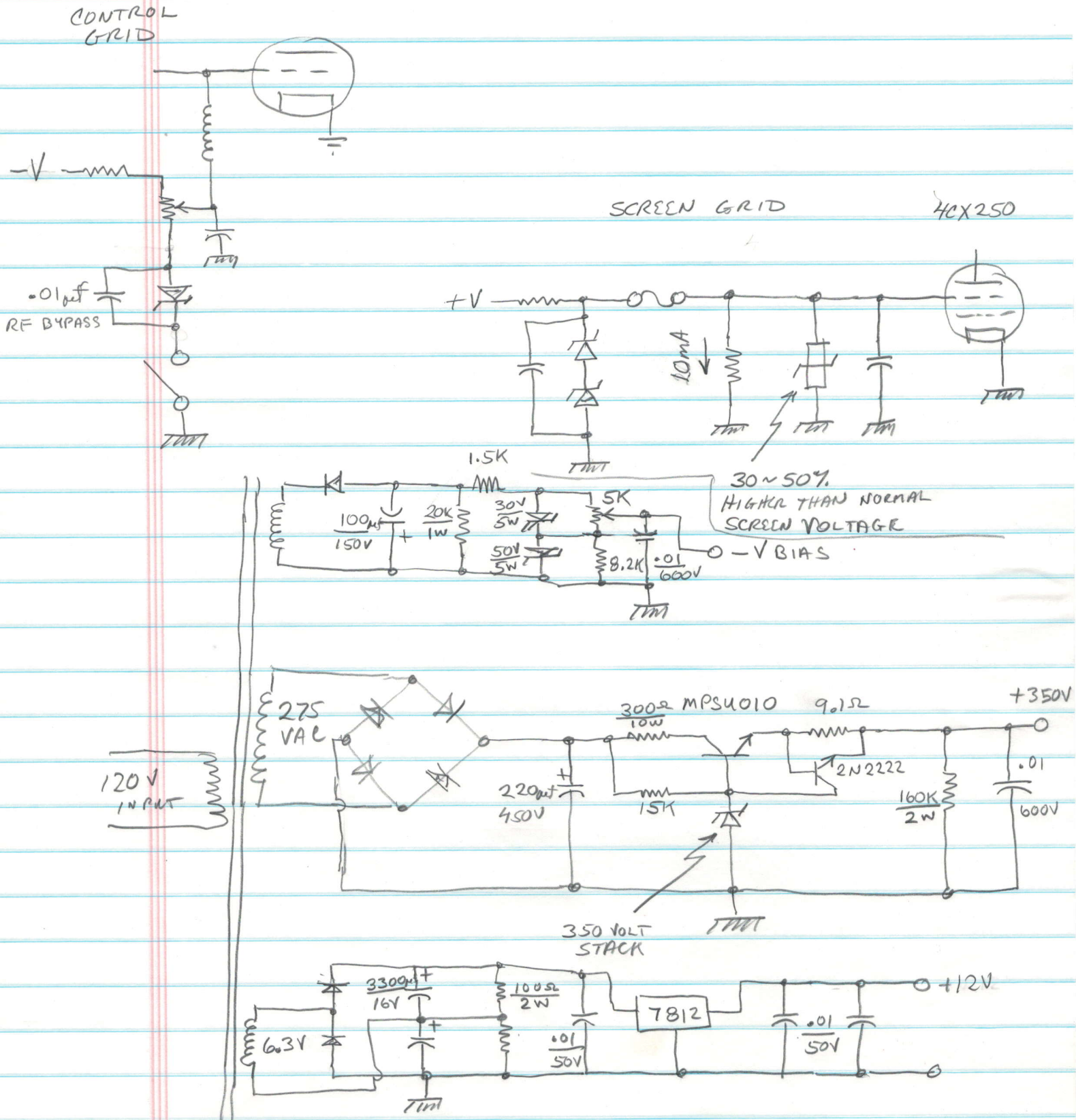
TRIAD N-470A ISOLATION XFMR



SCREEN SUPPLY

NEG. BIAS

4CX250 GRID SUPPLIES



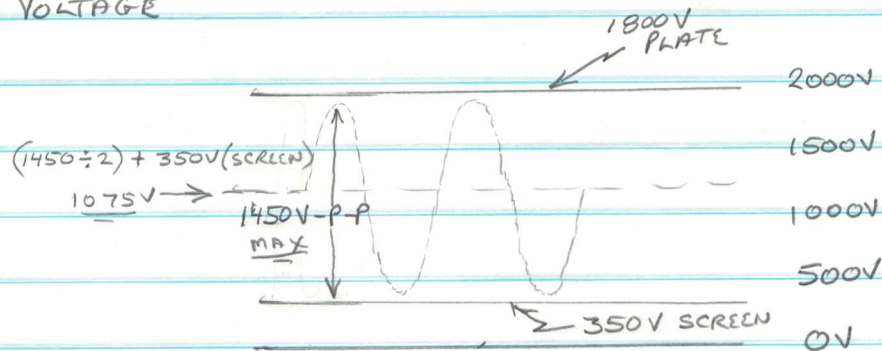
POWER AMPLIFIER FUNDAMENTALS

$$- i_p = g_m \times e_g -$$

WHERE: i_p = PLATE CURRENT

$$g_m = \text{TRANSCONDUCTANCE (mu)} \quad \Delta i_p / \Delta e_g$$

$$e_g = \text{GRID } \underline{RF} \text{ VOLTAGE}$$



— DETERMINE PLATE LOAD RESISTANCE —

OPTIMUM TUBE LOAD RESISTANCE =

$$R_L = \frac{V_P}{K \times I_P} \quad \text{WHERE:}$$

$$Q = \frac{X}{R}$$

R_L = THE APPROPRIATE LOAD RESISTANCE, IN OHMS

V_P = DC PLATE POTENTIAL, IN VOLTS

I_P = DC PLATE CURRENT, IN AMPS

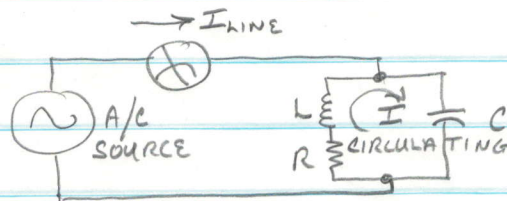
K = < A CONSTANT THAT APPROXIMATES THE RMS CURRENT FOR EACH CLASS OF OPERATION > :

CLASS A, $K \approx 1.3$

CLASS AB, $K \approx 1.5 \sim 1.7$

CLASS B, $K \approx 1.57 \sim 1.8$

CLASS C, $K \approx 2$



$$Q = \frac{X}{R}$$

— TANK CIRCUIT Q —

SINCE BOTH CIRCULATING CURRENT AND Q ARE PROPORTIONAL TO $1/R$, CIRCULATING CURRENT IS THEREFORE PROPORTIONAL TO Q . THE TANK CIRCULATING CURRENT THEREFORE EQUALS LINE CURRENT TIMES Q :

EX: IF LINE CURRENT = 100 mA & $Q = 10$; $I_{\text{CIRCULATING}} = 1 \text{ AMP!}$

— TANK Q. CONT. —

WHEN THERE IS NO LOAD CONNECTED TO THE TANK, THE ONLY RESISTANCES CONTRIBUTING TO R ARE THE LOSSES IN THE TANK CIRCUIT. THE "UNLOADED Q " (Q_u) IN THAT CASE IS:

$$Q_u = \frac{X}{R_{\text{LOSS}}}$$

WHERE: X = REACTANCE OF EITHER INDUCTOR OR CAPACITOR

R_{LOSS} = EFFECTIVE SERIES LOSS RESISTANCE IN THE CIRCUIT.

* A LOAD CONNECTED TO A TANK CIRCUIT HAS EXACTLY THE SAME EFFECT ON TANK OPERATION AS CIRCUIT LOSSES. (BOTH CONSUME ENERGY) CIRCUIT LOSSES BECOME HEAT RATHER THAN USEFUL OUTPUT.

WHEN ENERGY IS COUPLED OUT OF THE TANK TO A LOAD, THE LOADED Q (Q_L) IS:

$$Q_L = \frac{X}{R_{\text{LOSS}} + R_{\text{LOAD}}}$$

WHERE R_{LOAD} IS THE LOAD RESISTANCE. R_{LOSS} SHOULD BE AS SMALL AS PRACTICAL TO YIELD THE HIGHEST VALUE OF UNLOADED Q .

$$\text{TANK EFFICIENCY} = \frac{R_{\text{LOAD}}}{R_{\text{LOAD}} + R_{\text{LOSS}}} \times 100 = \%$$

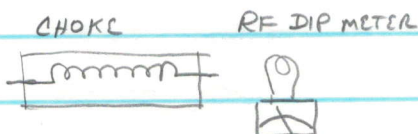
ALSO ALGEBRAICALLY:

$$\left(1 - \frac{Q_L}{Q_u}\right) \times 100$$

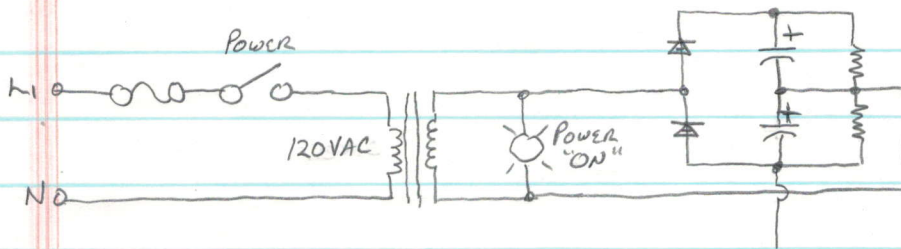
WHERE Q_L = TANK CIRCUIT LOADED Q

Q_u = UNLOADED Q OF THE TANK CIRCUIT.

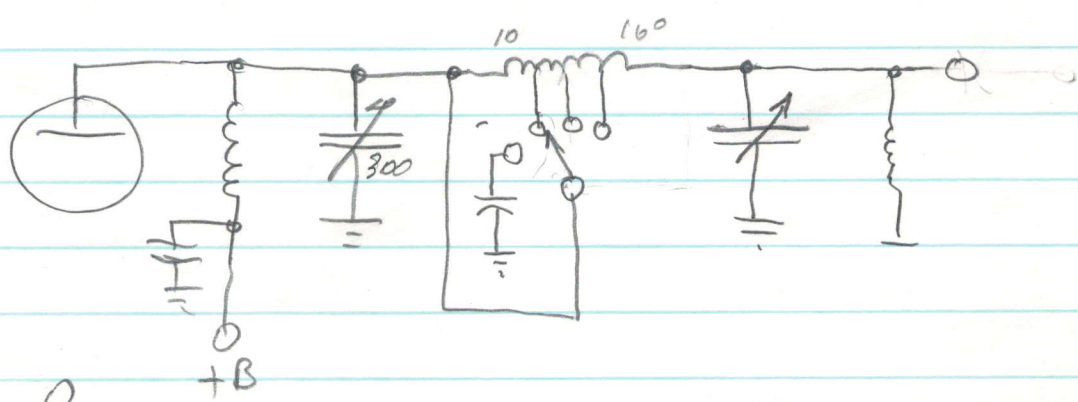
— RF CHOKES —



USE A DIP METER TO CHECK FOR UNWANTED RESONANT RISE NEAR ANY DESIRED OPERATING FREQUENCIES



- PAUL -
 W7KBE
 3885
 7:00-9:00 AM
 7282
 3:30-4:30



$$R = \frac{E}{I} = \frac{1800}{.5} = \frac{1800}{1.2}$$

